## FEATURES

12 MHz multiplying bandwidth
INL of $\pm 0.25$ LSB @ 8-bit
8-lead TSOT and MSOP packages
2.5 V to 5.5 V supply operation

Pin-compatible 8-/10-/12-/14-bit current output DACs
$\pm 10 \mathrm{~V}$ reference input
50 MHz serial interface
2.7 MSPS update rate

Extended temperature range: $-\mathbf{4 0}{ }^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
4-quadrant multiplication
Power-on reset with brownout detect
$<0.4 \mu \mathrm{~A}$ typical current consumption
Guaranteed monotonic

## APPLICATIONS

Portable battery-powered applications
Waveform generators
Analog processing
Instrumentation applications
Programmable amplifiers and attenuators
Digitally controlled calibration
Programmable filters and oscillators
Composite video
Ultrasound
Gain, offset, and voltage trimming

## GENERAL DESCRIPTION

The AD5450/AD5451/AD5452/AD5453 ${ }^{1}$ are CMOS 8-/10-/ 12-/14-bit current output digital-to-analog converters, respectively. These devices operate from a 2.5 V to 5.5 V power supply, making them suited to several applications, including battery-powered applications.

As a result of manufacture on a CMOS submicron process, these DACs offer excellent 4-quadrant multiplication characteristics of up to 12 MHz .

These DACs utilize a double-buffered, 3-wire serial interface that is compatible with SPI ${ }^{\ominus}$, QSPI $^{\mathrm{mw}}$, MICROWIRE ${ }^{\mathrm{mm}}$, and most DSP interface standards. Upon power-up, the internal shift register and latches are filled with 0 s , and the DAC output is at zero scale.

FUNCTIONAL BLOCK DIAGRAM


Figure 1.

The applied external reference input voltage ( $\mathrm{V}_{\text {REF }}$ ) determines the full-scale output current. These parts can handle $\pm 10 \mathrm{~V}$ inputs on the reference, despite operating from a single-supply power supply of 2.5 V to 5.5 V . An integrated feedback resistor ( $\mathrm{R}_{\mathrm{FB}}$ ) provides temperature tracking and full-scale voltage output when combined with an external current-to-voltage precision amplifier.

The AD5450/AD5451/AD5452/AD5453 DACs are available in small 8-lead TSOT, and the AD5452/AD5453 are also available in MSOP packages.

[^0]Rev. B
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## AD5450/AD5451/AD5452/AD5453

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## SPECIFICATIONS

$\mathrm{V}_{\mathrm{DD}}=2.5 \mathrm{~V}$ to $5.5 \mathrm{~V}, \mathrm{~V}_{\mathrm{REF}}=10 \mathrm{~V}$. Temperature range for Y version: $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. All specifications $\mathrm{T}_{\mathrm{MIN}}$ to $\mathrm{T}_{\mathrm{MAX}}$, unless otherwise noted. DC performance measured with OP177 and ac performance measured with AD8038, unless otherwise noted.
Table 1.

| Parameter | Min | Typ | Max | Unit | Conditions |
| :---: | :---: | :---: | :---: | :---: | :---: |
| STATIC PERFORMANCE |  |  |  |  |  |
| AD5450 |  |  |  |  |  |
| Resolution |  |  | 8 | Bits |  |
| Relative Accuracy |  |  | $\pm 0.25$ | LSB |  |
| Differential Nonlinearity |  |  | $\pm 0.5$ | LSB | Guaranteed monotonic |
| Total Unadjusted Error |  |  | $\pm 0.5$ | LSB |  |
| Gain Error |  |  | $\pm 0.25$ | LSB |  |
| AD5451 |  |  |  |  |  |
| Resolution |  |  | 10 | Bits |  |
| Relative Accuracy |  |  | $\pm 0.25$ | LSB |  |
| Differential Nonlinearity |  |  | $\pm 0.5$ | LSB | Guaranteed monotonic |
| Total Unadjusted Error |  |  | $\pm 0.5$ | LSB |  |
| Gain Error |  |  | $\pm 0.25$ | LSB |  |
| AD5452 |  |  |  |  |  |
| Resolution |  |  | 12 | Bits |  |
| Relative Accuracy |  |  | $\pm 0.5$ | LSB |  |
| Differential Nonlinearity |  |  | $\pm 1$ | LSB | Guaranteed monotonic |
| Total Unadjusted Error |  |  | $\pm 1$ | LSB |  |
| Gain Error |  |  | $\pm 0.5$ | LSB |  |
| AD5453 |  |  |  |  |  |
| ResolutionRelative Accuracy |  |  | 14 | Bits |  |
|  |  |  | $\pm 2$ | LSB |  |
| Differential Nonlinearity |  |  | -1/+2 | LSB | Guaranteed monotonic |
| Total Unadjusted Error |  |  | $\pm 4$ | LSB |  |
| Gain Error ${ }_{\text {Gain Error Temperature Coefficient }{ }^{1}}$ |  | $\pm 2$ | $\pm 2.5$ | LSB |  |
|  |  |  | ppm FSR/ $/{ }^{\circ} \mathrm{C}$ |  |
| Output Leakage Current |  |  |  | $\pm 1$ | nA | Data $=0 \times 0000, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, lout 1 |
|  |  |  | $\pm 10$ | nA | Data $=0 \times 0000, \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$, lout 1 |
| REFERENCE INPUT ${ }^{1}$ |  |  |  |  |  |
| Reference Input Range |  | $\pm 10$ |  | V |  |
| $V_{\text {ReF }}$ Input Resistance | 7 | 9 | 11 | k $\Omega$ | Input resistance, $\mathrm{TC}=-50 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| RFB Feedback Resistance | 7 | 9 | 11 | $\mathrm{k} \Omega$ | Input resistance, $\mathrm{TC}=-50 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| Input Capacitance |  |  |  |  |  |
| Zero-Scale Code |  | 18 | 22 | pF |  |
| Full-Scale Code |  | 18 | 22 | pF |  |
| DIGITAL INPUTS/OUTPUTS ${ }^{1}$ |  |  |  |  |  |
| Input High Voltage, $\mathrm{V}_{\mathbf{I H}}$ | 2.0 |  |  | V | $\mathrm{V}_{\mathrm{DD}}=3.6 \mathrm{~V}$ to 5 V |
|  | 1.7 |  |  | V | $V_{D D}=2.5 \mathrm{~V}$ to 3.6 V |
| Input Low Voltage, V $\mathrm{V}_{\text {IL }}$ |  |  | 0.8 | V | $\mathrm{V}_{\mathrm{DD}}=2.7 \mathrm{~V}$ to 5.5 V |
|  |  |  | 0.7 | V | $\mathrm{V}_{\mathrm{DD}}=2.5 \mathrm{~V}$ to 2.7 V |
| Output High Voltage, $\mathrm{V}_{\text {о }}$ | $V_{\text {DD }}-1$ |  |  | V | $\mathrm{V}_{\text {dD }}=4.5 \mathrm{~V}$ to 5 V , ISOURCE $=200 \mu \mathrm{~A}$ |
|  | $V_{D D}-0.5$ |  |  | V | $\mathrm{V}_{\mathrm{DD}}=2.5 \mathrm{~V}$ to 3.6 V , I IoURCE $=200 \mu \mathrm{~A}$ |
| Output Low Voltage, Vol |  |  | 0.4 | V | $\mathrm{V}_{\text {DD }}=4.5 \mathrm{~V}$ to 5 V , $\mathrm{I}_{\text {SIINK }}=200 \mu \mathrm{~A}$ |
|  |  |  | 0.4 | V | $\mathrm{V}_{\mathrm{DD}}=2.5 \mathrm{~V}$ to 3.6 V , $\mathrm{I}_{\text {IINK }}=200 \mu \mathrm{~A}$ |
| Input Leakage Current, IIL |  |  | $\pm 1$ | nA | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |
|  |  |  | $\pm 10$ | nA | $\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Input Capacitance |  |  | 10 | pF |  |

## AD5450/AD5451/AD5452/AD5453

| Parameter | Min | Typ | Max | Unit | Conditions |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| Reference-Multiplying BW |  | 12 |  | MHz | $\mathrm{V}_{\text {REF }}= \pm 3.5 \mathrm{~V}$, DAC loaded with all 1 s |
| Multiplying Feedthrough Error |  |  |  |  | $\mathrm{V}_{\text {REF }}= \pm 3.5 \mathrm{~V}$, DAC loaded with all 0 s |
|  |  | 72 |  | dB | 100 kHz |
|  |  | 64 |  | dB | 1 MHz |
|  |  | 44 |  | dB | 10 MHz |
| Output Voltage Settling Time |  |  |  |  | $V_{\text {REF }}=10 \mathrm{~V}$, RLoAd $=100 \Omega$; DAC latch alternately loaded with 0 s and 1 s |
| Measured to $\pm 1 \mathrm{mV}$ of FS |  | 100 | 110 | ns |  |
| Measured to $\pm 4 \mathrm{mV}$ of FS |  | 24 | 40 | ns |  |
| Measured to $\pm 16 \mathrm{mV}$ of FS |  | 16 | 33 | ns |  |
| Digital Delay |  | 20 | 40 | ns | Interface delay time |
| 10\% to 90\% Settling Time |  | 10 | 30 | ns | Rise and fall times, $\mathrm{V}_{\text {REF }}=10 \mathrm{~V}, \mathrm{RLOAD}=100 \Omega$ |
| Digital-to-Analog Glitch Impulse |  | 2 |  | $n \mathrm{~V}$-s | 1 LSB change around major carry, $\mathrm{V}_{\mathrm{REF}}=0 \mathrm{~V}$ |
| Output Capacitance |  |  |  |  |  |
| lout1 |  | 13 |  | pF | DAC latches loaded with all 0s |
|  |  | 28 |  | pF | DAC latches loaded with all 1 s |
| lout2 |  | 18 |  | pF | DAC latches loaded with all 0s |
|  |  | 5 |  |  | DAC latches loaded with all 1 s |
| Digital Feedthrough |  | 0.5 |  | nV -s | Feedthrough to DAC output with $\overline{C S}$ high and alternate loading of all 0 s and all 1 s |
| Analog THD |  | 83 |  | dB | $\begin{aligned} & V_{\text {REF }}=3.5 \mathrm{~V} \mathrm{p-p}, \text { all } 1 \mathrm{~s} \text { loaded, } \mathrm{f}=1 \mathrm{kHz} \\ & \text { Clock }=1 \mathrm{MHz}, \mathrm{~V}_{\text {REF }}=3.5 \mathrm{~V} \end{aligned}$ |
| Digital THD |  |  |  |  |  |
| 50 kHz fout |  | 71 |  | dB | Clock $=1 \mathrm{MHz}, \mathrm{V}_{\text {REF }}=3.5 \mathrm{~V}$ |
| 20 kHz fout |  | 77 |  | dB |  |
| Output Noise Spectral Density |  | 25 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ | @ 1 kHzClock $=1 \mathrm{MHz}, \mathrm{V}_{\text {REF }}=3.5 \mathrm{~V}$ |
| SFDR Performance (Wide Band) |  |  |  |  |  |
| 50 kHz fout |  | 78 |  | dB | Clock $=1 \mathrm{MHz}, \mathrm{V}_{\text {REF }}=3.5 \mathrm{~V}$ |
| 20 kHz fout |  | 74 |  | dB |  |
| SFDR Performance (Narrow Band) |  |  |  |  | Clock $=1 \mathrm{MHz}, \mathrm{V}_{\text {ReF }}=3.5 \mathrm{~V}$ |
| 50 kHz fout |  | 87 |  | dB |  |
| 20 kHz fout |  | 85 |  | dB |  |
| Intermodulation Distortion |  | 79 |  | dB | $\mathrm{f}_{1}=20 \mathrm{kHz}, \mathrm{f}_{2}=25 \mathrm{kHz}$, clock $=1 \mathrm{MHz}, \mathrm{V}_{\text {REF }}=3.5 \mathrm{~V}$ |
| POWER REQUIREMENTS |  |  |  |  |  |
| Power Supply Range | 2.5 |  | 5.5 | V |  |
| IDD |  | 0.4 | 10 | $\mu \mathrm{A}$ | $\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$, logic inputs $=0 \mathrm{~V}$ or $\mathrm{V}_{\mathrm{DD}}$ |
|  |  |  | 0.6 | $\mu \mathrm{A}$ | $\mathrm{T}_{\text {A }}=25^{\circ} \mathrm{C}$, logic inputs $=0 \mathrm{~V}$ or $\mathrm{V}_{\mathrm{DD}}$ |
| Power Supply Sensitivity ${ }^{1}$ |  |  | 0.001 | \%/\% | $\Delta V_{D D}= \pm 5 \%$ |

[^1]
## AD5450/AD5451/AD5452/AD5453

## TIMING CHARACTERISTICS

All input signals are specified with $t_{R}=t_{F}=1 \mathrm{~ns}\left(10 \%\right.$ to $90 \%$ of $\left.V_{\mathrm{DD}}\right)$ and timed from a voltage level of $\left(\mathrm{V}_{\mathrm{IL}}+\mathrm{V}_{\mathrm{IH}}\right) / 2 . \mathrm{V}_{\mathrm{DD}}=2.5 \mathrm{~V}$ to 5.5 V , $\mathrm{V}_{\text {Ref }}=10 \mathrm{~V}$, temperature range for Y version: $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. All specifications $\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\mathrm{MAX}}$, unless otherwise noted.
Table 2.

| Parameter ${ }^{1}$ | $\mathrm{V}_{\mathrm{DD}}=2.5 \mathrm{~V}$ to 5.5 V | Unit | Conditions/Comments |
| :---: | :---: | :---: | :---: |
| $\mathrm{f}_{\text {scık }}$ | 50 | MHz max | Maximum clock frequency |
| $\mathrm{t}_{1}$ | 20 | ns min | SCLK cycle time |
| $\mathrm{t}_{2}$ | 8 | $n s$ min | SCLK high time |
| $\mathrm{t}_{3}$ | 8 | ns min | SCLK low time |
| $\mathrm{t}_{4}$ | 8 | $n \mathrm{nsmin}$ | $\overline{\text { SYNC }}$ falling edge to SCLK active edge setup time |
| $\mathrm{t}_{5}$ | 5 | $n \mathrm{nmin}$ | Data setup time |
| $\mathrm{t}_{6}$ | 4.5 | $n s$ min | Data hold time |
| $\mathrm{t}_{7}$ | 5 | $n \mathrm{nmin}$ | $\overline{\text { SYNC }}$ rising edge to SCLK active edge |
| $\mathrm{t}_{8}$ | 30 | ns min | Minimum $\overline{\text { SYNC }}$ high time |
| Update Rate | 2.7 | MSPS | Consists of cycle time, $\overline{\text { SYNC }}$ high time, data setup, and output voltage settling time |

${ }^{1}$ Guaranteed by design and characterization, not subject to production test.


Figure 2. Timing Diagram

## AD5450/AD5451/AD5452/AD5453

## ABSOLUTE MAXIMUM RATINGS

Transient currents of up to 100 mA do not cause SCR latch-up. $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.

Table 3.

| Parameter | Rating |
| :---: | :---: |
| $V_{\text {DD }}$ to GND | -0.3 V to +7V |
| $V_{\text {REF, }}$, $\mathrm{R}_{\text {fb }}$ to GND | -12 V to +12 V |
| lout1 to GND | -0.3 V to +7 V |
| Input Current to Any Pin Except Supplies | $\pm 10 \mathrm{~mA}$ |
| Logic Inputs and Output ${ }^{1}$ | -0.3 V to $\mathrm{V}_{\mathrm{DD}}+0.3 \mathrm{~V}$ |
| Operating Temperature Range, Extended (Y Version) | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Storage Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Junction Temperature | $150^{\circ} \mathrm{C}$ |
| $\theta_{\text {JA }}$ Thermal Impedance |  |
| 8-Lead MSOP | $206^{\circ} \mathrm{C} / \mathrm{W}$ |
| 8-Lead TSOT | $211^{\circ} \mathrm{C} / \mathrm{W}$ |
| Lead Temperature, Soldering (10 sec) | $300^{\circ} \mathrm{C}$ |
| IR Reflow, Peak Temperature ( $<20 \mathrm{sec} \mathrm{)}$ | $235^{\circ} \mathrm{C}$ |

${ }^{1}$ Overvoltages at SCLK, $\overline{\text { SYNC, and SDIN are clamped by internal diodes. }}$

## ESD CAUTION

ESD (electrostatic discharge) sensitive device. Electrostatic charges as high as 4000 V readily accumulate on the human body and test equipment and can discharge without detection. Although this product features proprietary ESD protection circuitry, permanent damage may occur on devices subjected to high energy electrostatic discharges. Therefore, proper ESD precautions are recommended to avoid performance degradation or loss of functionality.

## WARNING! जितitilit <br> ESD SENSITIVE DEVICE

## PIN CONFIGURATIONS AND FUNCTION DESCRIPTIONS



Figure 3. TSOT Pin Configuration


Figure 4. MSOP Pin Configuration

Table 4. Pin Function Descriptions

| Pin No. |  | Mnemonic | Description |
| :---: | :---: | :---: | :---: |
| TSOT | MSOP |  |  |
| 1 | 8 | R ${ }_{\text {fb }}$ | DAC Feedback Resistor. Establish voltage output for the DAC by connecting to external amplifier output. |
| 2 | 7 | $V_{\text {REF }}$ | DAC Reference Voltage Input. |
| 3 | 6 | V ${ }_{\text {D }}$ | Positive Power Supply Input. These parts can operate from a supply of 2.5 V to 5.5 V . |
| 4 | 5 | $\overline{\text { SYNC }}$ | Active Low Control Input. This is the frame synchronization signal for the input data. Data is loaded to the shift register upon the active edge of the following clocks. |
| 5 | 4 | SDIN | Serial Data Input. Data is clocked into the 16-bit input register upon the active edge of the serial clock input. By default, in power-up mode data is clocked into the shift register upon the falling edge of SCLK. The control bits allow the user to change the active edge to a rising edge. |
| 6 | 3 | SCLK | Serial Clock Input. By default, data is clocked into the input shift register upon the falling edge of the serial clock input. Alternatively, by means of the serial control bits, the device can be configured such that data is clocked into the shift register upon the rising edge of SCLK. |
| 7 | 2 | GND | Ground Pin. |
| 8 | 1 | lout1 | DAC Current Output. |

## AD5450/AD5451/AD5452/AD5453

## TYPICAL PERFORMANCE CHARACTERISTICS



Figure 5. INL vs. Code (8-Bit DAC)


Figure 6. INL vs. Code (10-Bit DAC)


Figure 7. INL vs. Code (12-Bit DAC)


Figure 8. INL vs. Code (14-Bit DAC)


Figure 9. DNL vs. Code (8-Bit DAC)


Figure 10. DNL vs. Code (10-Bit DAC)


Figure 11. DNL vs. Code (12-Bit DAC)


Figure 12. DNL vs. Code (14-Bit DAC)


Figure 13. INL vs. Reference Voltage


Figure 14. DNL vs. Reference Voltage


Figure 15. TUE vs. Code (8-Bit DAC)


Figure 16. TUE vs. Code (10-Bit DAC)

## AD5450/AD5451/AD5452/AD5453



Figure 17. TUE vs. Code (12-Bit DAC)


Figure 18. TUE vs. Code (14-Bit DAC)


Figure 19. TUE vs. Reference Voltage


Figure 20. Gain Error (LSB) vs. Temperature


Figure 21. Gain Error (LSB) vs. Reference Voltage


Figure 22. Iout1 Leakage Current vs. Temperature


Figure 23. Supply Current vs. Logic Input Voltage


Figure 24. Supply Current vs. Temperature


Figure 25. Supply Current vs. Update Rate


Figure 26. Threshold Voltage vs. Supply Voltage


Figure 27. Reference Multiplying Bandwidth vs. Frequency and Code


Figure 28. Reference Multiplying Bandwidth—All 1s Loaded

## AD5450/AD5451/AD5452/AD5453



Figure 29. Reference Multiplying Bandwidth vs. Frequency and Compensation Capacitor


Figure 30. Midscale Transition, $V_{R E F}=0 \mathrm{~V}$


Figure 31. Midscale Transition, $V_{\text {REF }}=3.5 \mathrm{~V}$


Figure 32. Power Supply Rejection Ratio vs. Frequency


Figure 33. THD + Noise vs. Frequency


Figure 34. Wideband SFDR vs. fout Frequency

## AD5450/AD5451/AD5452/AD5453



Figure 35. Wideband SFDR, fout $=20 \mathrm{kHz}$, Clock $=1 \mathrm{MHz}$


Figure 36. Wideband SFDR, fout $=50 \mathrm{kHz}$, Clock $=1 \mathrm{MHz}$


Figure 37. Narrow-Band SFDR, fout $=20 \mathrm{kHz}$, Clock $=1 \mathrm{MHz}$


Figure 38. Narrow-Band SFDR , fout $=50 \mathrm{kHz}$, Clock $=1 \mathrm{MHz}$

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Figure 39. Narrow-Band IMD, $f_{\text {OUT }}=20 \mathrm{kHz}, 25 \mathrm{kHz}$, Clock $=1 \mathrm{MHz}$


Figure 41. Output Noise Spectral Density


Figure 40. Wideband $I M D, f_{\text {Out }}=20 \mathrm{kHz}, 25 \mathrm{kHz}$, Clock $=1 \mathrm{MHz}$

## AD5450/AD5451/AD5452/AD5453

## TERMINOLOGY

## Relative Accuracy (Endpoint Nonlinearity)

A measure of the maximum deviation from a straight line passing through the endpoints of the DAC transfer function. It is measured after adjusting for zero and full scale and is normally expressed in LSBs or as a percentage of the full-scale reading.

## Differential Nonlinearity

The difference between the measured change and the ideal 1 LSB change between any two adjacent codes. A specified differential nonlinearity of -1 LSB maximum over the operating temperature range ensures monotonicity.

## Gain Error (Full-Scale Error)

A measure of the output error between an ideal DAC and the actual device output. For these DACs, ideal maximum output is $\mathrm{V}_{\text {Ref }}-1$ LSB. Gain error of the DACs is adjustable to zero with external resistance.

## Output Leakage Current

The current that flows into the DAC ladder switches when it is turned off. For the Iour 1 terminal, it can be measured by loading all 0 s to the DAC and measuring the Iour 1 current.

## Output Capacitance

Capacitance from Iour 1 to AGND.

## Output Current Settling Time

The amount of time it takes for the output to settle to a specified level for a full-scale input change. For these devices, it is specified with a $100 \Omega$ resistor to ground. The settling time specification includes the digital delay from the $\overline{\text { SYNC }}$ rising edge to the fullscale output change.

## Digital-to-Analog Glitch Impulse

The amount of charge injected from the digital inputs to the analog output when the inputs change state. This is normally specified as the area of the glitch in either pA-s or nV-s, depending on whether the glitch is measured as a current or voltage signal.

## Digital Feedthrough

When the device is not selected, high frequency logic activity on the device's digital inputs may be capacitively coupled through the device and produce noise on the Iout pins. This noise is coupled from the outputs of the device onto follow-on circuitry. This noise is digital feedthrough.

## Multiplying Feedthrough Error

The error due to capacitive feedthrough from the DAC reference input to the DAC Iout 1 terminal when all 0 s are loaded to the DAC.

## Total Harmonic Distortion (THD)

The DAC is driven by an ac reference. The ratio of the rms sum of the harmonics of the DAC output to the fundamental value is the THD. Usually only the lower-order harmonics, such as second to fifth, are included.

$$
T H D=20 \log \frac{\sqrt{V_{2}^{2}+V_{3}{ }^{2}+V_{4}{ }^{2}+V_{5}^{2}}}{V_{1}}
$$

## Digital Intermodulation Distortion (IMD)

Second-order intermodulation measurements are the relative magnitudes of the fa and fb tones generated digitally by the DAC and the second-order products at $2 \mathrm{fa}-\mathrm{fb}$ and $2 \mathrm{fb}-\mathrm{fa}$.

## Compliance Voltage Range

The maximum range of (output) terminal voltage for which the device provides the specified characteristics.

## Spurious-Free Dynamic Range (SFDR)

The usable dynamic range of a DAC before spurious noise interferes or distorts the fundamental signal. SFDR is the measure of difference in amplitude between the fundamental and the largest harmonically or nonharmonically related spur from dc to full Nyquist bandwidth (half the DAC sampling rate or $\mathrm{f}_{\mathrm{s}} / 2$ ). Narrow-band SFDR is a measure of SFDR over an arbitrary window size, in this case $50 \%$ of the fundamental. Digital SFDR is a measure of the usable dynamic range of the DAC when the signal is a digitally generated sine wave.

## AD5450/AD5451/AD5452/AD5453

## GENERAL DESCRIPTION

## DAC SECTION

The AD5450/AD5451/AD5452/AD5453 are 8-/10-/12-/14-bit current output DACs, respectively, consisting of a segmented (4-bit) inverting R-2R ladder configuration. A simplified diagram for the 12-bit AD5452 is shown in Figure 42.


Figure 42. AD5452 Simplified Ladder
The feedback resistor, $\mathrm{R}_{\mathrm{Fb}}$, has a value of R . The value of R is typically $9 \mathrm{k} \Omega$ (with a minimum value of $7 \mathrm{k} \Omega$ and a maximum value of $11 \mathrm{k} \Omega$ ). If Iour 1 is kept at the same potential as GND, a constant current flows in each ladder leg, regardless of digital input code. Therefore, the input resistance presented at $\mathrm{V}_{\text {ref }}$ is always constant and nominally of value R. The DAC output (Iout1) is code-dependent, producing various resistances and capacitances. When choosing the external amplifier, take into account the variation in impedance generated by the DAC on the amplifier's inverting input node.

Access is provided to the $\mathrm{V}_{\mathrm{REF}}, \mathrm{R}_{\mathrm{FB}}$, and Iout1 terminals of the DAC, making the device extremely versatile and allowing it to be configured in several operating modes; for example, it can provide a unipolar output or can provide 4-quadrant multiplication in bipolar mode. Note that a matching switch is used in series with the internal $R_{F B}$ feedback resistor. If users attempt to measure $\mathrm{R}_{\mathrm{FB}}$, power must be applied to $\mathrm{V}_{\mathrm{DD}}$ to achieve continuity.

## CIRCUIT OPERATION

## Unipolar Mode

Using a single op amp, these devices can easily be configured to provide a 2-quadrant multiplying operation or a unipolar output voltage swing, as shown in Figure 43. When an output amplifier is connected in unipolar mode, the output voltage is given by

$$
V_{O U T}=-\frac{D}{2^{n}} \times V_{R E F}
$$

where:
$D$ is the fractional representation of the digital word loaded to the DAC.
$D=0$ to 255 (8-bit AD5450).

$$
=0 \text { to } 1023 \text { (10-bit AD5451). }
$$

$n$ is the number of bits.

Note that the output voltage polarity is opposite to the $\mathrm{V}_{\mathrm{REF}}$ polarity for dc reference voltages.


Figure 43. Unipolar Mode Operation
These DACs are designed to operate with either negative or positive reference voltages. The $V_{D D}$ power pin is only used by the internal digital logic to drive the on and off states of the DAC switches.

These DACs are designed to accommodate ac reference input signals in the range of -10 V to +10 V .

With a fixed 10 V reference, the circuit shown in Figure 43 gives a unipolar 0 V to -10 V output voltage swing. When $\mathrm{V}_{\text {IN }}$ is an ac signal, the circuit performs 2-quadrant multiplication.

Table 5 shows the relationship between the digital code and the expected output voltage for a unipolar operation using the 8 -bit AD5450.

Table 5. Unipolar Code Table for the AD5450

| Digital Input | Analog Output (V) |
| :--- | :--- |
| 11111111 | $-V_{\text {REF }}(255 / 256)$ |
| 10000000 | $-V_{\text {REF }}(128 / 256)=-V_{\text {REF }} / 2$ |
| 00000001 | $-V_{\text {REF }}(1 / 256)$ |
| 00000000 | $-V_{\text {REF }}(0 / 256)=0$ |

$$
=0 \text { to } 4095 \text { (12-bit AD5452). }
$$

$$
=0 \text { to 16,383 (14-bit AD5453). }
$$

## AD5450/AD5451/AD5452/AD5453

## Bipolar Mode

In some applications, it may be necessary to generate a full 4-quadrant multiplying operation or a bipolar output swing. This can be easily accomplished by using another external amplifier and some external resistors, as shown in Figure 44. In this circuit, the second amplifier, A2, provides a gain of 2. Biasing the external amplifier with an offset from the reference voltage results in full 4-quadrant multiplying operation. The transfer function of this circuit shows that both negative and positive output voltages are created as the input data (D) is incremented from Code 0 ( $\mathrm{V}_{\text {out }}=-\mathrm{V}_{\text {REFF }}$ ) to midscale $\left(V_{\text {out }}-0 \mathrm{~V}\right)$ to full scale $\left(\mathrm{V}_{\text {out }}=+\mathrm{V}_{\text {ref }}\right)$.

$$
V_{\text {OUT }}=\left(V_{R E F} \times \frac{D}{2^{n-1}}\right)-V_{R E F}
$$

where:
$D$ is the fractional representation of the digital word loaded to the DAC.
$D=0$ to 255 (8-bit AD5450).

$$
=0 \text { to } 1023 \text { (10-bit AD5451). }
$$

$$
=0 \text { to } 4095 \text { (12-bit AD5452). }
$$

$n$ is the resolution of the DAC.

When $\mathrm{V}_{\text {IN }}$ is an ac signal, the circuit performs 4-quadrant multiplication. Table 6 shows the relationship between the digital code and the expected output voltage for a bipolar operation using the 8-bit AD5450.

Table 6. Bipolar Code Table for the AD5450

| Digital Input | Analog Output (V) |
| :--- | :--- |
| 11111111 | $+V_{\text {REF }}(127 / 128)$ |
| 10000000 | 0 |
| 00000001 | $-V_{\text {REF }}(127 / 128)$ |
| 00000000 | $-V_{\text {REF }}(128 / 128)$ |

$n$ is resolution of


Figure 44. Bipolar Mode Operation (4-Quadrant Multiplication)

## AD5450/AD5451/AD5452/AD5453

## Stability

In the I-to-V configuration, the Iout of the DAC and the inverting node of the op amp must be connected as close as possible, and proper PCB layout techniques must be employed. Because every code change corresponds to a step function, gain peaking may occur if the op amp has limited gain bandwidth product (GBP) and there is excessive parasitic capacitance at the inverting node. This parasitic capacitance introduces a pole into the open-loop response, which can cause ringing or instability in the closed-loop applications circuit.

An optional compensation capacitor, C 1 , can be added in parallel with $\mathrm{R}_{\mathrm{FB}}$ for stability, as shown in Figure 43 and Figure 44. Too small a value of C 1 can produce ringing at the output, and too large a value can adversely affect the settling time. C1 should be found empirically, but 1 pF to 2 pF is generally adequate for the compensation.

## SINGLE-SUPPLY APPLICATIONS

## Voltage-Switching Mode

Figure 45 shows these DACs operating in the voltage-switching mode. The reference voltage, $\mathrm{V}_{\text {IN }}$, is applied to the $\mathrm{I}_{\text {out }} 1 \mathrm{pin}$, and the output voltage is available at the $\mathrm{V}_{\text {ref }}$ terminal. In this configuration, a positive reference voltage results in a positive output voltage, making single-supply operation possible. The output from the DAC is voltage at a constant impedance (the DAC ladder resistance); therefore, an op amp is necessary to buffer the output voltage. The reference input no longer sees constant input impedance, but one that varies with code; therefore, the voltage input should be driven from a low impedance source.


It is important to note that with this configuration $V_{\text {IN }}$ is limited to low voltages because the switches in the DAC ladder do not have the same source-drain drive voltage. As a result, their on resistance differs, which degrades the integral linearity of the DAC. Also, VIN must not go negative by more than 0.3 V , or an internal diode turns on, causing the device to exceed the maximum ratings. In this type of application, the full range of multiplying capability of the DAC is lost.

## Positive Output Voltage

The output voltage polarity is opposite to the $\mathrm{V}_{\text {REF }}$ polarity for dc reference voltages. To achieve a positive voltage output, an applied negative reference to the input of the DAC is preferred over the output inversion through an inverting amplifier because of the resistors' tolerance errors. To generate a negative reference, the reference can be level-shifted by an op amp such that the Vout and GND pins of the reference become the virtual ground and -2.5 V , respectively, as shown in Figure 46.


Figure 46. Positive Output Voltage with Minimum Components

## ADDING GAIN

In applications in which the output voltage is required to be greater than $\mathrm{V}_{\mathrm{IN}}$, gain can be added with an additional external amplifier, or it can be achieved in a single stage. It is important to consider the effect of the temperature coefficients of the DAC's thin film resistors. Simply placing a resistor in series with the $\mathrm{R}_{\mathrm{FB}}$ resistor causes mismatches in the temperature coefficients and results in larger gain temperature coefficient errors. Instead, increase the gain of the circuit by using the recommended configuration shown in Figure 47. R1, R2, and R3 should have similar temperature coefficients, but they need not match the temperature coefficients of the DAC. This approach is recommended in circuits where gains greater than 1 are required.


Figure 47. Increasing Gain of Current-Output DAC

## AD5450/AD5451/AD5452/AD5453

## DIVIDER OR PROGRAMMABLE GAIN ELEMENT

Current-steering DACs are very flexible and lend themselves to many different applications. If this type of DAC is connected as the feedback element of an op amp and $\mathrm{R}_{\mathrm{FB}}$ is used as the input resistor as shown in Figure 48, the output voltage is inversely proportional to the digital input fraction, D.

For $D=1-2^{-n}$, the output voltage is

$$
V_{O U T}=\frac{-V_{I N}}{D}=\frac{-V_{I N}}{\left(1-2^{-n}\right)}
$$

As D is reduced, the output voltage increases. For small values of the digital fraction, D , it is important to ensure that the amplifier does not saturate and that the required accuracy is met. For example, an 8-bit DAC driven with the binary code $0 x 10$ (00010000), that is, 16 decimal, in the circuit of Figure 48 should cause the output voltage to be 16 times $\mathrm{V}_{\text {IN }}$.


Figure 48. Current-Steering DAC Used as a Divider or Programmable Gain Element

However, if the DAC has a linearity specification of $\pm 0.5$ LSB, D can have weight anywhere in the range of $15.5 / 256$ to $16.5 / 256$. Therefore, the possible output voltage is in the range of $15.5 \mathrm{~V}_{\mathrm{IN}}$ to $16.5 \mathrm{~V}_{\mathrm{IN}}$-an error of $3 \%$, even though the DAC itself has a maximum error of $0.2 \%$.

DAC leakage current is also a potential error source in divider circuits. The leakage current must be counterbalanced by an opposite current supplied from the op amp through the DAC. Because only a fraction, D , of the current in the $\mathrm{V}_{\text {ref }}$ terminal is routed to the Iour 1 terminal, the output voltage changes as follows:

$$
\text { Output Error Voltage Due to Leakage }=(\text { Leakage } \times R) / D
$$

where $R$ is the DAC resistance at the $\mathrm{V}_{\text {Ref }}$ terminal.
For a DAC leakage current of $10 \mathrm{nA}, \mathrm{R}=10 \mathrm{k} \Omega$, and a gain (that is, $1 / \mathrm{D}$ ) of 16 , the error voltage is 1.6 mV .

## REFERENCE SELECTION

When selecting a reference for use with this series of currentoutput DACs, pay attention to the reference's output voltage
temperature coefficient specification. This parameter not only affects the full-scale error, but also may affect the linearity (INL and DNL) performance. The reference temperature coefficient should be consistent with the system accuracy specifications. For example, an 8 -bit system is required to hold its overall specification to within 1 LSB over the temperature range $0^{\circ} \mathrm{C}$ to $50^{\circ} \mathrm{C}$, and the system's maximum temperature drift should be less than $78 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$.

A 12-bit system within 2 LSB accuracy requires a maximum drift of $10 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$. Choosing a precision reference with a low output temperature coefficient minimizes this error source. Table 7 lists some dc references available from Analog Devices that are suitable for use with this range of current-output DACs.

## AMPLIFIER SELECTION

The primary requirement for the current-steering mode is an amplifier with low input bias currents and low input offset voltage. The input offset voltage of an op amp is multiplied by the variable gain of the circuit due to the code-dependent output resistance of the DAC. A change in this noise gain between two adjacent digital fractions produces a step change in the output voltage due to the offset voltage of the amplifier's input. This output voltage change is superimposed on the desired change in output between the two codes and gives rise to a differential linearity error, which if large enough, could cause the DAC to be nonmonotonic.

The input bias current of an op amp generates an offset at the voltage output as a result of the bias current flowing in the feedback resistor, $\mathrm{R}_{\text {Fb. }}$. Most op amps have input bias currents low enough to prevent significant errors in 12-bit applications. However, for 14-bit applications, some consideration should be given to selecting an appropriate amplifier.

Common-mode rejection of the op amp is important in voltageswitching circuits because it produces a code-dependent error at the voltage output of the circuit. Most op amps have adequate common-mode rejection for use at $8-, 10-$, and 12 -bit resolutions.

Provided that the DAC switches are driven from true wideband low impedance sources ( $\mathrm{V}_{\mathrm{IN}}$ and AGND), they settle quickly. Consequently, the slew rate and settling time of a voltageswitching DAC circuit is determined largely by the output op amp. To obtain minimum settling time in this configuration, it is important to minimize capacitance at the $V_{\text {ref }}$ node (the voltage output node in this application) of the DAC. This is done by using low input-capacitance buffer amplifiers and careful board design.

Most single-supply circuits include ground as part of the analog signal range, which in turn requires an amplifier that can handle rail-to-rail signals. There is a large range of singlesupply amplifiers available from Analog Devices.

## AD5450/AD5451/AD5452/AD5453

Table 7. Suitable ADI Precision References

| Part No. | Output Voltage (V) | Initial Tolerance (\%) | Temp Drift (ppm/ ${ }^{\circ} \mathbf{C}$ ) | Iss (mA) | Output Noise $(\boldsymbol{\mu} \mathbf{V} \mathbf{p - p})$ | Package |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| ADR01 | 10 | 0.05 | 3 | 1 | 20 |  |
| ADR01 | 10 | 0.05 | 9 | 1 | 20 | SOIC-8 |
| ADR02 | 5 | 0.06 | 3 | 1 | 10 | TSOT-23, SC70 |
| ADR02 | 5 | 0.06 | 9 | 1 | SOIC-8 |  |
| ADR03 | 2.5 | 0.10 | 3 | 1 | TSOT-23, SC70 |  |
| ADR03 | 2.5 | 0.10 | 9 | 1 | SOIC-8 |  |
| ADR06 | 3 | 0.10 | 3 | 6 | TSOT-23, SC70 |  |
| ADR06 | 3 | 0.10 | 9 | 1 | SOIC-8 |  |
| ADR431 | 2.5 | 0.04 | 3 | 10 | TSOT-23, SC70 |  |
| ADR435 | 5 | 0.04 | 9 | 0 | SOIC-8 |  |
| ADR391 | 2.5 | 0.16 | 9 | 0.8 | SOIC-8 |  |
| ADR395 | 5 | 0.10 | 0.12 | 8 | TSOT-23 |  |

Table 8. Suitable ADI Precision Op Amps

| Part No. | Supply Voltage (V) | Vos (Max) ( $\mu \mathrm{V}$ ) | $\mathrm{I}_{\mathrm{B}}(\mathrm{Max})(\mathrm{nA})$ | $\begin{aligned} & 0.1 \mathrm{~Hz} \text { to } 10 \mathrm{~Hz} \\ & \text { Noise ( } \mu \mathrm{V} \text { p-p) } \end{aligned}$ | Supply Current ( $\mu \mathrm{A}$ ) | Package |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OP97 | $\pm 2$ to $\pm 20$ | 25 | 0.1 | 0.5 | 600 | SOIC-8 |
| OP1177 | $\pm 2.5$ to $\pm 15$ | 60 | 2 | 0.4 | 500 | MSOP, SOIC-8 |
| AD8551 | 2.7 to 5 | 5 | 0.05 | 1 | 975 | MSOP, SOIC-8 |
| AD8603 | 1.8 to 6 | 50 | 0.001 | 2.3 | 50 | TSOT |
| AD8628 | 2.7 to 6 | 5 | 0.1 | 0.5 | 850 | TSOT, SOIC-8 |

Table 9. Suitable ADI High Speed Op Amps

| Part No. | Supply Voltage (V) | BW @ ACL (MHz) | Slew Rate (V/ $\boldsymbol{\mu s})$ | VOS $(\mathbf{M a x})(\boldsymbol{\mu V})$ | $\mathbf{I}_{\mathbf{B}}(\mathbf{M a x})$ ( $\mathbf{n A}$ ) | Package |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| AD8065 | 5 to 24 | 145 | 180 | 1500 | 0.006 | SOIC-8, SOT-23, MSOP |
| AD8021 | $\pm 2.5$ to $\pm 12$ | 490 | 120 | 1000 | 10500 | SOIC-8, MSOP |
| AD8038 | 3 to 12 | 350 | 425 | 3000 | 750 | SOIC-8, SC70-5 |
| AD9631 | $\pm 3$ to $\pm 6$ | 320 | 1300 | 7000 | SOIC-8 |  |

## SERIAL INTERFACE

The AD5450/AD5451/AD5452/AD5453 have an easy-to-use 3-wire interface that is compatible with SPI, QSPI, MICROWIRE, and most DSP interface standards. Data is written to the device in 16 -bit words. This 16 -bit word consists of two control bits and 8 , 10, 12, or 14 data bits, as shown in Figure 49, Figure 50, Figure 51, and Figure 52. The AD5453 uses all 14 bits of DAC data, the AD5452 uses 12 bits and ignores the two LSBs, the AD5451 uses 10 bits and ignores the four LSBs, and the AD5450 uses 8 bits and ignores the six LSBs.

## DAC Control Bits C1, C0

Control Bits C 1 and C 0 allow the user to load and update the new DAC code and to change the active clock edge. By default, the shift register clocks data upon the falling edge; this can be changed via the control bits. If changed, the DAC core is inoperative until the next data frame. A power cycle resets the core to default condition. On-chip power-on reset circuitry ensures that the device powers on with zero scale loaded to the DAC register and Iout line.

Table 10. DAC Control Bits

| C1 | C0 | Function Implemented |
| :--- | :--- | :--- |
| 0 | 0 | Load and update (power-on default) |
| 0 | 1 | Reserved |
| 1 | 0 | Reserved |
| 1 | 1 | Clock data to shift register upon rising edge |

## $\overline{\text { SYNC Function }}$

$\overline{\text { SYNC }}$ is an edge-triggered input that acts as a framesynchronization signal and chip enable. Data can only be transferred to the device while $\overline{\text { SYNC }}$ is low. To start the serial data transfer, $\overline{\text { SYNC }}$ should be taken low, observing the minimum $\overline{\text { SYNC }}$ falling to SCLK falling edge setup time, $\mathrm{t}_{4}$. To minimize the power consumption of the device, the interface powers up fully only when the device is being written to, that is, upon the falling edge of $\overline{\text { SYNC. The SCLK and SDIN input }}$ buffers are powered down upon the rising edge of $\overline{S Y N C}$.

After the falling edge of the $16^{\text {th }}$ SCLK pulse, bring $\overline{\text { SYNC }}$ high to transfer data from the input shift register to the DAC register.


Figure 49. AD5450 8-Bit Input Shift Register Contents


Figure 50. AD5451 10-Bit Input Shift Register Contents


Figure 52. AD5453 14-Bit Input Shift Register Contents

## MICROPROCESSOR INTERFACING

Microprocessor interfacing to a AD5450/AD5451/AD5452/ AD5453 DAC is through a serial bus that uses standard protocol and is compatible with microcontrollers and DSP processors. The communication channel is a 3-wire interface consisting of a clock signal, a data signal, and a synchronization signal. The AD5450/AD5451/AD5452/AD5453 require a 16-bit word, with the default being data valid upon the falling edge of SCLK, but this is changeable using the control bits in the data-word.

## ADSP-21xx-toAD5450/AD5451/AD5452/AD5453 Interface

The ADSP-21xx family of DSPs is easily interfaced to a AD5450/AD5451/AD5452/AD5453 DAC without the need for extra glue logic. Figure 53 is an example of an SPI interface between the DAC and the ADSP-2191M. SCK of the DSP drives the serial data line, SDIN. $\overline{\text { SYNC }}$ is driven from one of the port lines, in this case $\overline{\text { SPIxSEL. }}$


Figure 53. ADSP-2191 SPI-to-AD5450/AD5451/AD5452/AD5453 Interface
A serial interface between the DAC and DSP SPORT is shown in Figure 54. In this example, SPORT0 is used to transfer data to the DAC shift register. Transmission is initiated by writing a word to the Tx register after the SPORT has been enabled. In a write sequence, data is clocked out upon each rising edge of the DSP's serial clock and clocked into the DAC input shift register upon the falling edge of its SCLK. The update of the DAC output takes place upon the rising edge of the $\overline{\text { SYNC }}$ signal.

## AD5450/AD5451/AD5452/AD5453



Figure 54. ADSP-2101/ADSP-2103/ADSP-2191
SPORT-to-AD5450/AD5451/AD5452/AD5453 Interface
Communication between two devices at a given clock speed is possible when the following specifications are compatible: frame $\overline{\text { SYNC }}$ delay and frame $\overline{\text { SYNC }}$ setup-and-hold, data delay and data setup-and-hold, and SCLK width. The DAC interface expects a $\mathrm{t}_{4}$ (SYNC falling edge to SCLK falling edge setup time) of 13 ns minimum. See the ADSP-21xx User Manual for information on clock and frame $\overline{\text { SYNC }}$ frequencies for the SPORT register. Table 11 shows the setup for the SPORT control register.

Table 11. SPORT Control Register Setup

| Name | Setting | Description |
| :--- | :--- | :--- |
| TFSW | 1 | Alternate framing |
| INVTFS | 1 | Active low frame signal |
| DTYPE | 00 | Right justify data |
| ISCLK | 1 | Internal serial clock |
| TFSR | 1 | Frame every word |
| ITFS | 1 | Internal framing signal |
| SLEN | 1111 | 16-bit data-word |

## ADSP-BF5xx-toAD5450/AD5451/AD5452/AD5453 Interface

The ADSP-BF5xx family of processors has an SPI-compatible port that enables the processor to communicate with SPIcompatible devices. A serial interface between the BlackFin ${ }^{*}$ processor and the AD5450/AD5451/AD5452/AD5453 DAC is shown in Figure 55. In this configuration, data is transferred through the MOSI (master output, slave input) pin. $\overline{\text { SYNC }}$ is driven by the $\overline{\text { SPIxSEL }}$ pin, which is a reconfigured programmable flag pin.


Figure 55. ADSP-BF5xx-to-AD5450/AD5451/AD5452/AD5453 Interface
The ADSP-BF5xx processor incorporates channel synchronous serial ports (SPORT). A serial interface between the DAC and the DSP SPORT is shown in Figure 56. When the SPORT is enabled, initiate transmission by writing a word to the Tx
register. The data is clocked out upon each rising edge of the DSP's serial clock and clocked into the DAC's input shift register upon the falling edge its SCLK. The DAC output is updated by using the transmit frame synchronization (TFS) line to provide a $\overline{\text { SYNC }}$ signal.


Figure 56. ADSP-BF5xx SPORT-to-AD5450/AD5451/AD5452/AD5453 Interface

## 80C51/80L51-to-

 AD5450/AD5451/AD5452/AD5453 InterfaceA serial interface between the DAC and the 80C51/80L51 is shown in Figure 57. TxD of the 80C51/80L51 drives SCLK of the DAC serial interface, and RxD drives the serial data line, SDIN. P1.1 is a bit-programmable pin on the serial port and is used to drive $\overline{\mathrm{SYNC}}$. As data is transmitted to the switch, P1.1 is taken low. The 80C51/80L51 transmit data only in 8 -bit bytes; therefore, only eight falling clock edges occur in the transmit cycle.

To load data correctly to the DAC, P1.1 is left low after the first eight bits are transmitted, and a second write cycle is initiated to transmit the second byte of data. Data on RxD is clocked out of the microcontroller upon the rising edge of TxD and is valid upon the falling edge. As a result, no glue logic is required between the DAC and microcontroller interface. P1.1 is taken high following the completion of this cycle. The 80C51/80L51 provide the LSB of its SBUF register as the first bit in the data stream. The DAC input register acquires its data with the MSB as the first bit received. The transmit routine should take this into account.


Figure 57. 80C51/80L51-to-AD5450/AD5451/AD5452/AD5453 Interface

## MC68HC11-to- <br> AD5450/AD5451/AD5452/AD5453 Interface

Figure 58 is an example of a serial interface between the DAC and the MC68HC11 microcontroller. The serial peripheral interface (SPI) on the MC68HC11 is configured for master mode $(\mathrm{MSTR})=1$, clock polarity bit $(\mathrm{CPOL})=0$, and clock phase bit $(\mathrm{CPHA})=1$. The SPI is configured by writing to the SPI control register (SPCR); see the 68HC11 User Manual. SCK of the $68 \mathrm{HC11}$ drives the SCLK of the DAC interface; the MOSI output drives the serial data line (SDIN) of the DAC.

The SYNC signal is derived from a port line (PC7). When data is being transmitted to the AD5450/AD5451/AD5452/AD5453, the $\overline{\text { SYNC }}$ line is taken low (PC7). Data appearing on the MOSI output is valid upon the falling edge of SCK. Serial data from the $68 \mathrm{HC1} 1$ is transmitted in 8-bit bytes with only eight falling clock edges occurring in the transmit cycle. Data is transmitted MSB first. To load data to the DAC, PC7 is left low after the first eight bits are transferred, and a second serial write operation is performed to the DAC. PC7 is taken high at the end of this procedure.

| MC68HC11*  <br>   <br> PC7  <br> SCK  <br> MOSI  |
| :--- |

Figure 58. MC68HC11-to-AD5450/AD5451/AD5452/AD5453 Interface
If the user wants to verify the data previously written to the input shift register, the SDO line can be connected to MISO of the MC68HC11. In this configuration with $\overline{\text { SYNC }}$ low, the shift register clocks data out upon the rising edges of SCLK.

## MICROWIRE-toAD5450/AD5451/AD5452/AD5453 Interface

Figure 59 shows an interface between the DAC and any MICROWIRE-compatible device. Serial data is shifted out upon the falling edge of the serial clock, SK, and is clocked into the DAC input shift register upon the rising edge of SK, which corresponds to the falling edge of the DAC's SCLK.


Figure 59. MICROWIRE-to-AD5450/AD5451/AD5452/AD5453 Interface

## PIC16C6x/PIC16C7x-toAD5450/AD5451/AD5452/AD5453 Interface

The PIC16C6x/PIC16C7x synchronous serial port (SSP) is configured as an SPI master with the clock polarity bit $(C K P)=0$. This is done by writing to the synchronous serial port control register (SSPCON); see the PIC16/PIC17 Microcontroller User Manual.

In this example, I/O Port RA1 is used to provide a $\overline{\text { SYNC }}$ signal and enable the serial port of the DAC. This microcontroller transfers only eight bits of data during each serial transfer operation; therefore, two consecutive write operations are required. Figure 60 shows the connection diagram.


Figure 60. PIC16C6x/7x-to-AD5450/AD5451/AD5452/AD5453 Interface

## PCB LAYOUT AND POWER SUPPLY DECOUPLING

In any circuit where accuracy is important, careful consideration of the power supply and ground return layout helps to ensure the rated performance. The printed circuit board on which a AD5450/AD5451/AD5452/AD5453 DAC is mounted should be designed so that the analog and digital sections are separated and confined to certain areas of the board. If the DAC is in a system where multiple devices require an AGND-to-DGND connection, the connection should be made at one point only. The star ground point should be established as close as possible to the device.

These DACs should have ample supply bypassing of $10 \mu \mathrm{~F}$ in parallel with $0.1 \mu \mathrm{~F}$ on the supply located as close to the package as possible, ideally right up against the device. The $0.1 \mu \mathrm{~F}$ capacitor should have low effective series resistance (ESR) and low effective series inductance (ESI), like the common ceramic types that provide a low impedance path to ground at high frequencies, to handle transient currents due to internal logic switching. Low ESR $1 \mu \mathrm{~F}$ to $10 \mu \mathrm{~F}$ tantalum or electrolytic capacitors should also be applied at the supplies to minimize transient disturbance and filter out low frequency ripple.

Components, such as clocks, that produce fast switching signals should be shielded with a digital ground to avoid radiating noise to other parts of the board, and they should never be run near the reference inputs.

Avoid crossover of digital and analog signals. Traces on opposite sides of the board should run at right angles to each other. This reduces the effects of feedthrough through the board. A microstrip technique is the best solution, but its use is not always possible with a double-sided board. In this technique, the component side of the board is dedicated to the ground plane and signal traces are placed on the solder side.

It is good practice to employ compact, minimum lead length PCB layout design. Leads to the input should be as short as possible to minimize IR drops and stray inductance.

The PCB metal traces between $V_{\text {REF }}$ and $R_{F B}$ should also be matched to minimize gain error. To optimize high frequency performance, the I-to-V amplifier should be located as close to the device as possible.

## AD5450/AD5451/AD5452/AD5453

## EVALUATION BOARD FOR THE DAC

The evaluation board consists of an AD5450, AD5451, AD5452, or AD5453 DAC and a current-to-voltage amplifier, such as an AD8065. Included on the evaluation board is a 10 V reference, ADR01. An external reference can also be applied via an SMB input.

The evaluation kit consists of a CD with PC software to control the DAC. The software allows the user to write code to the device.

## POWER SUPPLIES FOR THE EVALUATION BOARD

The board requires $\pm 12 \mathrm{~V}$ and +5 V supplies. The +12 V VDD and $-12 \mathrm{~V}_{\text {ss }}$ are used to power the output amplifier; the +5 V is used to power the DAC $\left(\mathrm{V}_{\mathrm{DDI}}\right)$ and transceivers $\left(\mathrm{V}_{\mathrm{CC}}\right)$.

Both supplies are decoupled to their respective ground plane with $10 \mu \mathrm{~F}$ tantalum and $0.1 \mu \mathrm{~F}$ ceramic capacitors.



Figure 62. Component-Side Artwork


Figure 63. Silkscreen-Component-Side View (Top)

## AD5450/AD5451/AD5452/AD5453



Figure 64. Solder-Side Artwork
Table 12. Overview of AD54xx and AD55xx Devices

| Part No. | Resolution | No. DACs | INL (LSB) | Interface | Package ${ }^{1}$ | Features |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AD5424 | 8 | 1 | $\pm 0.25$ | Parallel | RU-16, CP-20 | 10 MHz BW, $17 \mathrm{~ns} \overline{\mathrm{CS}}$ pulse width |
| AD5426 | 8 | 1 | $\pm 0.25$ | Serial | RM-10 | 10 MHz BW, 50 MHz serial |
| AD5428 | 8 | 2 | $\pm 0.25$ | Parallel | RU-20 | $10 \mathrm{MHz} \mathrm{BW}, 17 \mathrm{~ns} \overline{\mathrm{CS}}$ pulse width |
| AD5429 | 8 | 2 | $\pm 0.25$ | Serial | RU-10 | $10 \mathrm{MHz} \mathrm{BW}, 50 \mathrm{MHz}$ serial |
| AD5450 | 8 | 1 | $\pm 0.25$ | Serial | UJ-8 | $12 \mathrm{MHZ} \mathrm{BW}, 50 \mathrm{MHz}$ serial interface |
| AD5432 | 10 | 1 | $\pm 0.5$ | Serial | RM-10 | 10 MHz BW, 50 MHz serial |
| AD5433 | 10 | 1 | $\pm 0.5$ | Parallel | RU-20, CP-20 | $10 \mathrm{MHz} \mathrm{BW}, 17 \mathrm{~ns} \overline{\mathrm{CS}}$ pulse width |
| AD5439 | 10 | 2 | $\pm 0.5$ | Serial | RU-16 | 10 MHz BW, 50 MHz serial |
| AD5440 | 10 | 2 | $\pm 0.5$ | Parallel | RU-24 | $10 \mathrm{MHz} \mathrm{BW}, 17 \mathrm{~ns} \overline{\mathrm{CS}}$ pulse width |
| AD5451 | 10 | 1 | $\pm 0.25$ | Serial | UJ-8 | $12 \mathrm{MHz} \mathrm{BW}$,50 MHz serial interface |
| AD5443 | 12 | 1 | $\pm 1$ | Serial | RM-10 | 10 MHz BW, 50 MHz serial |
| AD5444 | 12 | 1 | $\pm 0.5$ | Serial | RM-10 | 12 MHz BW, 50 MHz serial |
| AD5415 | 12 | 2 | $\pm 1$ | Serial | RU-24 | 10 MHz BW, 50 MHz serial |
| AD5405 | 12 | 2 | $\pm 1$ | Parallel | CP-40 | $10 \mathrm{MHz} \mathrm{BW}, 17 \mathrm{~ns} \overline{\mathrm{CS}}$ pulse width |
| AD5445 | 12 | 2 | $\pm 1$ | Parallel | RU-20, CP-20 | $10 \mathrm{MHz} \mathrm{BW}, 17 \mathrm{~ns} \overline{\mathrm{CS}}$ pulse width |
| AD5447 | 12 | 2 | $\pm 1$ | Parallel | RU-24 | $10 \mathrm{MHz} \mathrm{BW}, 17 \mathrm{~ns} \overline{\mathrm{CS}}$ pulse width |
| AD5449 | 12 | 2 | $\pm 1$ | Serial | RU-16 | $10 \mathrm{MHz} \mathrm{BW}, 50 \mathrm{MHz}$ serial |
| AD5452 | 12 | 1 | $\pm 0.5$ | Serial | UJ-8, RM-8 | $12 \mathrm{MHz} \mathrm{BW}$,50 MHz serial interface |
| AD5446 | 14 | 1 | $\pm 1$ | Serial | RM-10 | 12 MHz BW, 50 MHz serial |
| AD5453 | 14 | 1 | $\pm 2$ | Serial | UJ-8, RM-8 | $12 \mathrm{MHz} \mathrm{BW}, 50 \mathrm{MHz}$ serial |
| AD5553 | 14 | 1 | $\pm 1$ | Serial | RM-8 | $4 \mathrm{MHz} \mathrm{BW}, 50 \mathrm{MHz}$ serial clock |
| AD5556 | 14 | 1 | $\pm 1$ | Parallel | RU-28 | $4 \mathrm{MHz} \mathrm{BW}, 20 \mathrm{~ns} \overline{\mathrm{WR}}$ pulse width |
| AD5555 | 14 | 2 | $\pm 1$ | Serial | RM-8 | $4 \mathrm{MHz} \mathrm{BW}, 50 \mathrm{MHz}$ serial clock |
| AD5557 | 14 | 2 | $\pm 1$ | Parallel | RU-38 | $4 \mathrm{MHz} \mathrm{BW}, 20 \mathrm{~ns} \overline{\mathrm{WR}}$ pulse width |
| AD5543 | 16 | 1 | $\pm 2$ | Serial | RM-8 | $4 \mathrm{MHz} \mathrm{BW}, 50 \mathrm{MHz}$ serial clock |
| AD5546 | 16 | 1 | $\pm 2$ | Parallel | RU-28 | 4 MHz BW, $20 \mathrm{n} \overline{\mathrm{WR}}$ pulse width |
| AD5545 | 16 | 2 | $\pm 2$ | Serial | RU-16 | $4 \mathrm{MHz} \mathrm{BW}, 50 \mathrm{MHz}$ serial clock |
| AD5547 | 16 | 2 | $\pm 2$ | Parallel | RU-38 | $4 \mathrm{MHz} \mathrm{BW}, 20 \mathrm{~ns} \overline{\mathrm{WR}}$ pulse width |

[^2]
## OUTLINE DIMENSIONS



Figure 66. 8-Lead Mini Small Outline Package [MSOP] (RM-8)
Dimensions shown in millimeters

## AD5450/AD5451/AD5452/AD5453

ORDERING GUIDE

| Model | Resolution | INL | Temperature Range | Package Description | Package Option | Branding |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AD5450YUJ-REEL | 8 | $\pm 0.25$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead TSOT | UJ-8 | D1X |
| AD5450YUJ-REEL7 | 8 | $\pm 0.25$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead TSOT | UJ-8 | D1X |
| AD5450YUJZ-REEL ${ }^{1}$ | 8 | $\pm 0.25$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead TSOT | UJ-8 | D6Y |
| AD5450YUJZ-REEL7 ${ }^{1}$ | 8 | $\pm 0.25$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead TSOT | UJ-8 | D6Y |
| AD5451YUJ-REEL | 10 | $\pm 0.25$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead TSOT | UJ-8 | D1Y |
| AD5451YUJ-REEL7 | 10 | $\pm 0.25$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead TSOT | UJ-8 | D1Y |
| AD5451YUJZ-REEL ${ }^{1}$ | 10 | $\pm 0.25$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead TSOT | UJ-8 | D6Z |
| AD5451YUJZ-REEL71 | 10 | $\pm 0.25$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead TSOT | UJ-8 | D6Z |
| AD5452YUJ-REEL | 12 | $\pm 0.5$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead TSOT | UJ-8 | D1Z |
| AD5452YUJ-REEL7 | 12 | $\pm 0.5$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead TSOT | UJ-8 | D1Z |
| AD5452YUJZ-REEL ${ }^{1}$ | 12 | $\pm 0.5$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead TSOT | UJ-8 | D70 |
| AD5452YUJZ-REEL7 ${ }^{1}$ | 12 | $\pm 0.5$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead TSOT | UJ-8 | D70 |
| AD5452YRM | 12 | $\pm 0.5$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | D1Z |
| AD5452YRM-REEL | 12 | $\pm 0.5$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | D1Z |
| AD5452YRM-REEL7 | 12 | $\pm 0.5$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | D1Z |
| AD5452YRMZ ${ }^{1}$ | 12 | $\pm 0.5$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | D70 |
| AD5452YRMZ-REEL ${ }^{1}$ | 12 | $\pm 0.5$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | D70 |
| AD5452YRMZ-REEL71 | 12 | $\pm 0.5$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | D70 |
| AD5453YUJ-REEL | 14 | $\pm 2$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead TSOT | UJ-8 | D26 |
| AD5453YUJ-REEL7 | 14 | $\pm 2$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead TSOT | UJ-8 | D26 |
| AD5453YRM | 14 | $\pm 2$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | D26 |
| AD5453YRM-REEL | 14 | $\pm 2$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | D26 |
| AD5453YRM-REEL7 | 14 | $\pm 2$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | D26 |
| EVAL-AD5450EB |  |  |  | Evaluation Kit |  |  |
| EVAL-AD5451EB |  |  |  | Evaluation Kit |  |  |
| EVAL-AD5452EB |  |  |  | Evaluation Kit |  |  |
| EVAL-AD5453EB |  |  |  | Evaluation Kit |  |  |

${ }^{1} \mathrm{Z}=\mathrm{Pb}$-free part.


[^0]:    ${ }^{1}$ U.S. Patent Number 5,689,257

[^1]:    ${ }^{1}$ Guaranteed by design and characterization, not subject to production test.

[^2]:    $\mathrm{RU}=\mathrm{TSSOP}, \mathrm{CP}=\mathrm{LFCSP}, \mathrm{RM}=\mathrm{MSOP}, \mathrm{UJ}=\mathrm{TSOT}$.

